

Modelling, Monitoring and Control of Biosystems

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A biological process is...

- The development (= growth) of micro-organisms (= biomass)
- By the consumption of a nutrient (= substrate)
- Under favourable environmental conditions : temperature, pH, stirring, aeration,...

Objectives :

1. Biomass production (e.g. baker's yeast)
2. Product synthesis (e.g. ethanol, biodegradable polymer, antibiotics, methane,...)
3. Waste-water treatment

R&D in biotechnology is aimed at improving productivity

3 approaches :

1. Microbiological/biochemical approach
 - selection of micro-organisms, nutrients,...
 - genetic modifications
2. Process engineering approach
 - operating modes/conditions
 - efficient techniques/processes
3. Process control/system theory approach
 - productivity maximisation via an on-line optimizing operation of the bioprocess
 - (on the basis of a dynamical model of the process)

There are two main obstacles for controlling bioprocesses

1. Modelling difficulties

- How to account for the numerous factors that influence the biochemical reactions (including the growth)?
- Nonlinear and non stationary models

2. Measuring difficulties

- Absence of cheap and reliable sensors for the key process variables

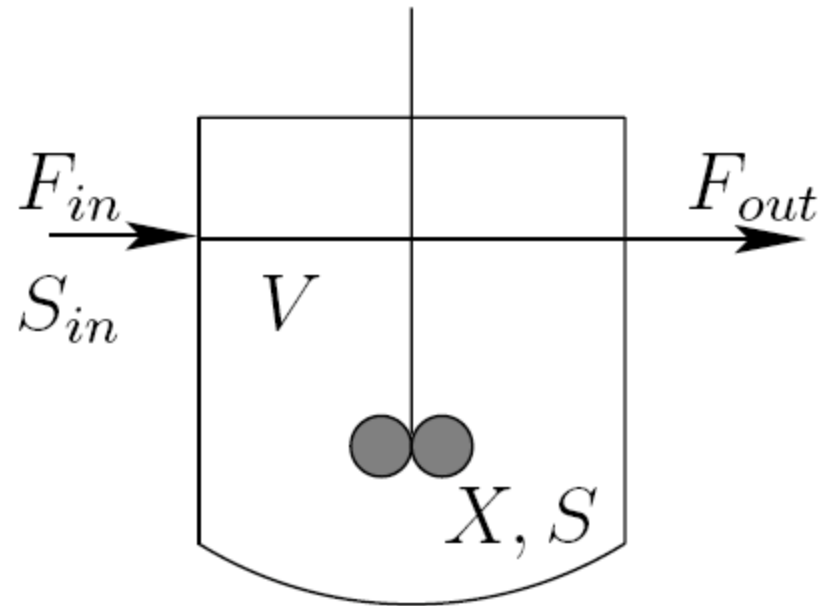
Outline

- Introduction
- Bioprocess models and model properties
- Parameter identification (including optimal experiment design)
- State estimation
- Some typical bioprocesses
- Numerical simulation and PDE's
- Control
 - optimal & adaptive extremum seeking control
 - specific issues in bioprocesses

Bioprocess models

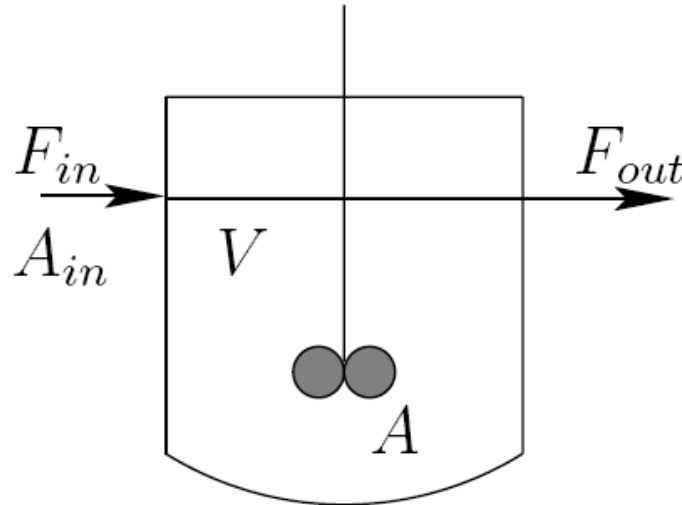
- The basic mathematical model
- The general dynamical model
- The reaction rates
- Extensions
 - link with metabolic engineering
 - population balance
 - microbial ecology
- Model properties

The basic mathematical model



- Autocatalytic reaction : $S \rightarrow X$
- Operating modes :
 - batch : $F_{in} = F_{out} = 0$
 - fed-batch : $F_{in} \neq 0, F_{out} = 0$
 - continuous : $F_{in} = F_{out}$ V constant

Notion of mass balance



Component A (substrate, product, biomass)

---> dynamical mass balance :

$$\left[\begin{array}{c} \text{time variation} \\ \text{of the mass} \\ \text{of A} \end{array} \right] = \left[\begin{array}{c} \text{mass inflow} \\ \text{of A into} \\ \text{the reactor} \end{array} \right] - \left[\begin{array}{c} \text{mass outflow} \\ \text{of A from} \\ \text{the reactor} \end{array} \right] - \left[\begin{array}{c} \text{mass of A} \\ \text{produced/} \\ \text{consumed} \\ \text{via reactions} \end{array} \right]$$

$$\frac{d(VA)}{dt} = F_{in}A_{in} - F_{out}A + Vr$$

Recall that :

$$\frac{d(VA)}{dt} = V \frac{dA}{dt} + A \frac{dV}{dt}$$

Therefore :

$$\frac{dA}{dt} = \frac{F_{in}}{V} A_{in} - \frac{F_{out}}{V} A - \frac{A}{V} \frac{dV}{dt} + r$$

- **batch** : $F_{in} = F_{out} = 0 \rightarrow V$ constant and $\frac{dV}{dt} = 0$

$$\rightarrow \frac{dA}{dt} = r$$

- **fed-batch** : $F_{out} = 0$ and $\frac{dV}{dt} = F_{in}$

$$\rightarrow \frac{dA}{dt} = \frac{F_{in}}{V} A_{in} - \frac{A}{V} \frac{dV}{dt} + r$$

- **continuous** : $F_{in} = F_{out} \neq 0$ and V constant

$$\rightarrow \frac{dA}{dt} = \frac{F_{in}}{V} A_{in} - \frac{F_{in}}{V} A + r$$

- Biomass growth :

$$\frac{dX}{dt} = \mu X - DX$$

- Substrate consumption :

$$\frac{dS}{dt} = -k_1 \mu X + DS_{in} - DS$$

- growth rate : μX
with μ : specific growth rate

- yield coefficient : k_1

- dilution rate : $D = \frac{F_{in}}{V}$

The dynamics of other components

- Liquid product (growth associated)

$$\frac{dP}{dt} = k_2\mu X - DP$$

P : liquid product concentration

- Gaseous product

$$Q = k_3\mu X$$

Q : gaseous product mass flowrate

- Aerobic cultures ----> (dissolved) oxygen

$$\frac{dC}{dt} = -k_4\mu X - DC + Q_{O_2,in} - Q_{O_2,out}$$

C : dissolved oxygen concentration

$Q_{O_2,in}$ $Q_{O_2,out}$: gaseous oxygen inlet and outlet flowrates

If the gas-liquid transfer is limiting :

$$Q_{O_2,in} - Q_{O_2,out} = k_L a (C_S - C)$$

$k_L a$: gas-liquid transfer coefficient

C_s : oxygen saturation concentration

The general dynamical model

$$\frac{dx}{dt} = \underbrace{K r(x)}_{\text{conversion}} + \underbrace{F - Q - Dx}_{\text{transport dynamics}}$$

x : vector of the concentrations

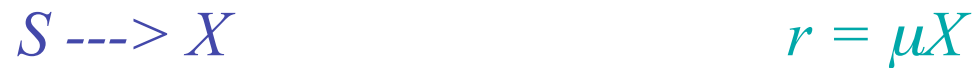
K : matrix of the stiochiometric coefficients

$r(x)$: vector of the reaction rates

F : vector of feeding rates

Q : vector of the produced gas flow rates

Example #1 : simple microbial growth



$$\begin{cases} x &= \begin{bmatrix} X \\ S \end{bmatrix}, K = \begin{bmatrix} 1 \\ -k_1 \end{bmatrix}, r = [\mu X] \\ F &= \begin{bmatrix} 0 \\ DS_{in} \end{bmatrix}, Q = 0 \end{cases}$$

General dynamical model

$$\frac{d}{dt} \begin{bmatrix} X \\ S \end{bmatrix} = -D \begin{bmatrix} X \\ S \end{bmatrix} + \begin{bmatrix} 1 \\ -k_1 \end{bmatrix} \mu X + \begin{bmatrix} 0 \\ DS_{in} \end{bmatrix}$$

Example #2 : two parallel reactions

Autocatalytic reaction : $S \xrightarrow{\mu} X$

$$r_1 = \mu X$$

Catalytic reaction : $S + X \xrightarrow{\nu} X + P$

$$r_2 = \nu X$$

(P in gaseous form)

Dynamical model :

$$\frac{dX}{dt} = \mu X - DX$$

$$\frac{dS}{dt} = -k_1 \mu X - k_2 \nu X + DS_{in} - DS$$

$$\frac{dP}{dt} = \nu X - DP - Q_1$$

Matrix form of the dynamical model :

$$\frac{d}{dt} \underbrace{\begin{bmatrix} X \\ S \\ P \end{bmatrix}}_x = -D \begin{bmatrix} X \\ S \\ P \end{bmatrix} + \underbrace{\begin{bmatrix} 1 & 0 \\ -k_1 & -k_2 \\ 0 & 1 \end{bmatrix}}_K \underbrace{\begin{bmatrix} \mu X \\ \nu X \end{bmatrix}}_r + \underbrace{\begin{bmatrix} 0 \\ DS_{in} \\ 0 \end{bmatrix}}_F - \underbrace{\begin{bmatrix} 0 \\ 0 \\ Q_1 \end{bmatrix}}_Q$$

Matrix K :

Column #1 = growth reaction

Column #2 = enzyme catalyzed reaction

+ standardisation of the yield coefficients

Example #3 : intracellular production of PHB

PHB = Poly- β -hydroxybutyric acid (biodegradable polymer)

Aerobic culture of *Alcaligenes eutrophus* in fedbatch reactor

- **2 limiting substrates :**
 - Source of carbone (fructose, glucose, ...)
 - Source of nitrogen (NH_4^+)
- **Intracellular production : 2 metabolic pathways :**
 - 1) associated to the growth (low yield)
 - 2) X catalysed by an enzyme (completely inhibited by N)
- **Bioreactor operation : 2 steps :**
 - 1) growth “without” production \rightarrow fed with both 2 substrates
 - 2) production without growth \rightarrow fed only with carbon

Dynamical model (mass balance)

Step #1 : growth “without” production

$$\frac{dX}{dt} = \mu X - DX$$

biomass

$$\frac{dS}{dt} = -k_1\mu X + DS_{in} - DS$$

carbon source

$$\frac{dN}{dt} = -k_2\mu X + DN_{in} - DN$$

nitrogen

$$\frac{dP}{dt} = k_3\mu X - DP$$

PHB

$$\frac{dC}{dt} = -k_4\mu X + Q_{in} - DC$$

oxygen

with

S_{in} , N_{in} : inlet concentration of S and N

Q_{in} : gaseous oxygen flowrate

Dynamical model (mass balance)(continued)

Step #2 : production without growth

$$\begin{aligned}\frac{dX}{dt} &= -DX && \text{biomass} \\ \frac{dS}{dt} &= -k_5\nu X + DS_{in} - DS && \text{carbon source} \\ N &= 0 && \text{nitrogen} \\ \frac{dP}{dt} &= \nu X - DP && \text{PHB} \\ \frac{dC}{dt} &= -k_6\nu X + Q_{in} - DC && \text{oxygen}\end{aligned}$$

with ν : specific production rate

PHB model : matrix form

Step #1

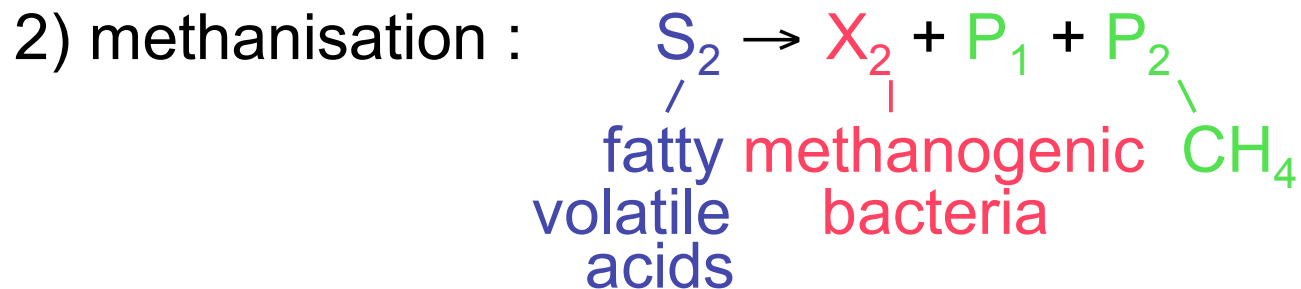
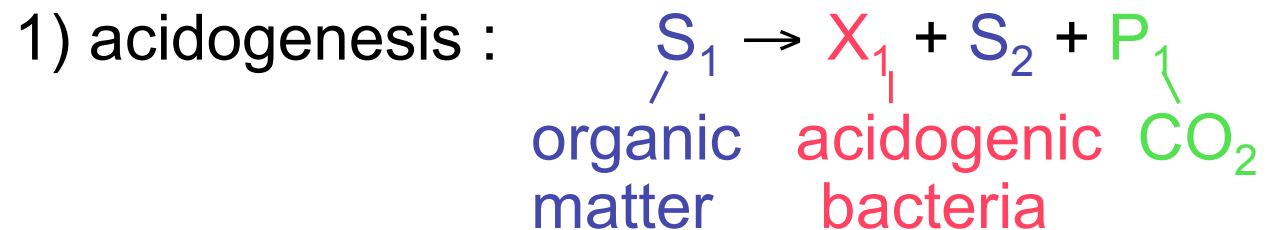
$$x = \begin{bmatrix} X \\ S \\ N \\ P \\ C \end{bmatrix}, K = \begin{bmatrix} 1 \\ -k_1 \\ -k_2 \\ k_3 \\ -k_4 \end{bmatrix}, F = \begin{bmatrix} 0 \\ DS_{in} \\ DN_{in} \\ 0 \\ Q_{in} \end{bmatrix}$$
$$r = [\mu X], Q = 0$$

Step #2

$$x = \begin{bmatrix} X \\ S \\ P \\ C \end{bmatrix}, K = \begin{bmatrix} 0 \\ -k_5 \\ 1 \\ -k_6 \end{bmatrix}, F = \begin{bmatrix} 0 \\ DS_{in} \\ 0 \\ Q_{in} \end{bmatrix}$$
$$r = [\nu X], Q = 0$$

Example #4 : anaerobic digestion (sequential reactions)

- Wastewater treatment with CH₄ production
- Complex process → simplified reaction scheme



Dynamical model (mass balance)

$$\begin{aligned}\frac{dX_1}{dt} &= \mu_1 X_1 - DX_1 \\ \frac{dS_1}{dt} &= -k_1 \mu_1 X_1 + DS_{in} - DS_1 \\ \frac{dX_2}{dt} &= \mu_2 X_2 - DX_2 \\ \frac{dS_2}{dt} &= k_3 \mu_1 X_1 - k_2 \mu_2 X_2 - DS_2 \\ \frac{dP_1}{dt} &= k_4 \mu_2 X_2 - DP_1 - Q_1 \\ \frac{dP_2}{dt} &= k_5 \mu_1 X_1 + k_6 \mu_2 X_2 - DP_2 - Q_2 \quad \text{CO}_2\end{aligned}$$

} acidogenesis

} methanisation

Anaerobic digestion model : matrix form

$$x = \begin{bmatrix} X_1 \\ S_1 \\ X_2 \\ S_2 \\ P_1 \\ P_2 \end{bmatrix}, K = \begin{bmatrix} 1 & 0 \\ -k_1 & 0 \\ 0 & 1 \\ k_3 & -k_2 \\ 0 & k_4 \\ k_5 & k_6 \end{bmatrix}, r = \begin{bmatrix} \mu_1 X_1 \\ \mu_2 X_2 \end{bmatrix}$$
$$F = \begin{bmatrix} 0 \\ DS_{in} \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}, Q = \begin{bmatrix} 0 \\ 0 \\ 0 \\ Q_1 \\ Q_2 \end{bmatrix}$$

The reaction rates

The specific growth rate may depend on

- the substrate concentration S
- the biomass concentration X
- the product concentration P
- the temperature T
- the pH pH
- the dissolved oxygen concentration C
- inhibitors' concentration I
- the light intensity L
- genetic modifications, ...

- Reaction rates : (nonlinear) functions of the process variables

A simple example : Monod microbial growth model

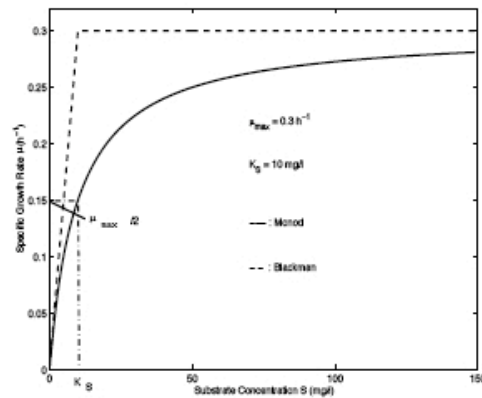
$$\mu_X = \frac{\mu_{max} S X}{K_S + S}$$

- But :
 - Choice of an appropriate model
(more than 60 models for μ !)
 - Calibration of the model parameters on the basis of the available experimental data
(identifiability issues)

μ depends on S, X, T, pH, ...

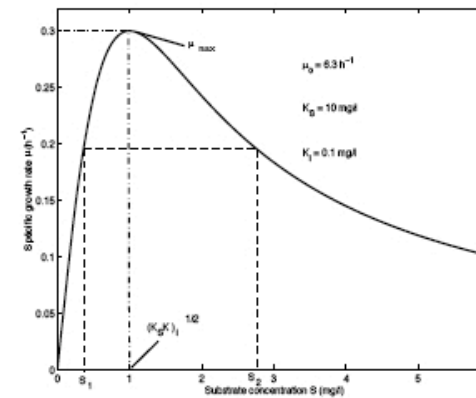
μ depends on S

Monod

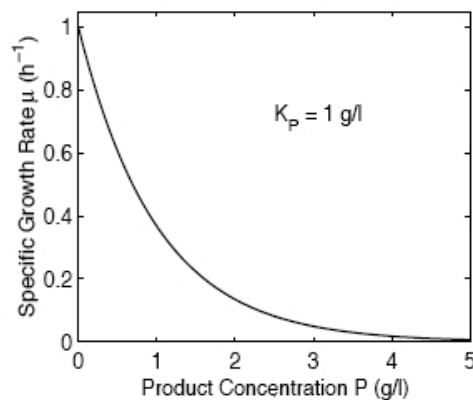


μ depends on S

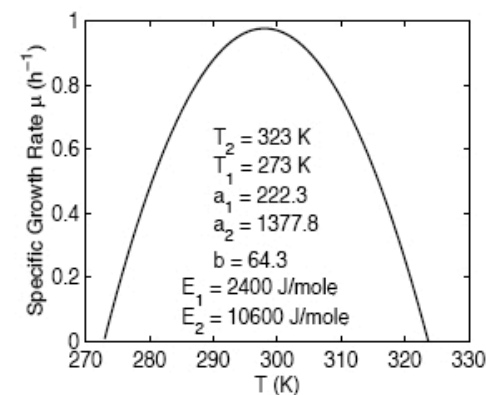
Haldane



μ depends on P



μ depends on T



Example : yeast growth

$$\mu(S, P, C) = \left(\frac{\mu_{1,max} S}{K_S + S} + \frac{\mu_{2,max} P}{K_P + P} \right) \left(\frac{C}{K_C + C} + K_1 C - K_2 \right)$$

- 7 parameters : $\mu_{1,max}$, $\mu_{2,max}$, K_S , K_P , K_C , K_1 , K_2
- If $S = 0$, $C = K_2/K_1$, $P \neq 0$, $X \neq 0$, $D = 0$:

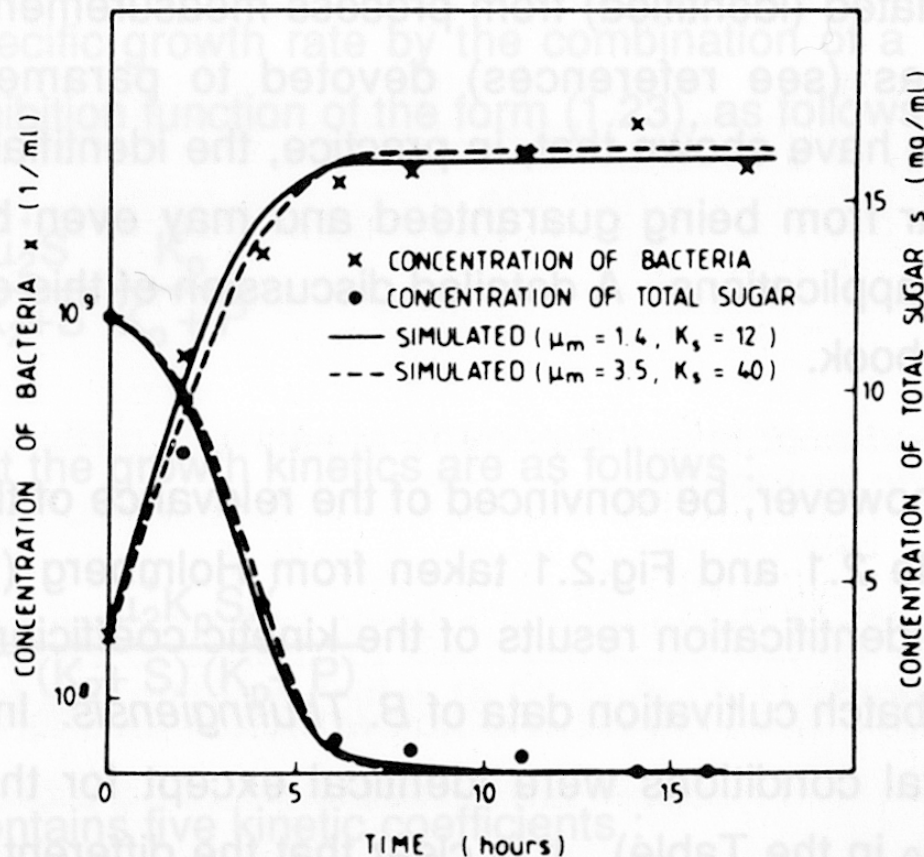
$$\frac{dS}{dt} = -k_1 \mu X + D S_{in} - D S$$

$$\longrightarrow \frac{dS}{dt} = -k_1 \frac{\mu_{2,max} P C}{(K_P + P)(K_C + C)} X < 0 !$$

physically absurd !
($S < 0$!)

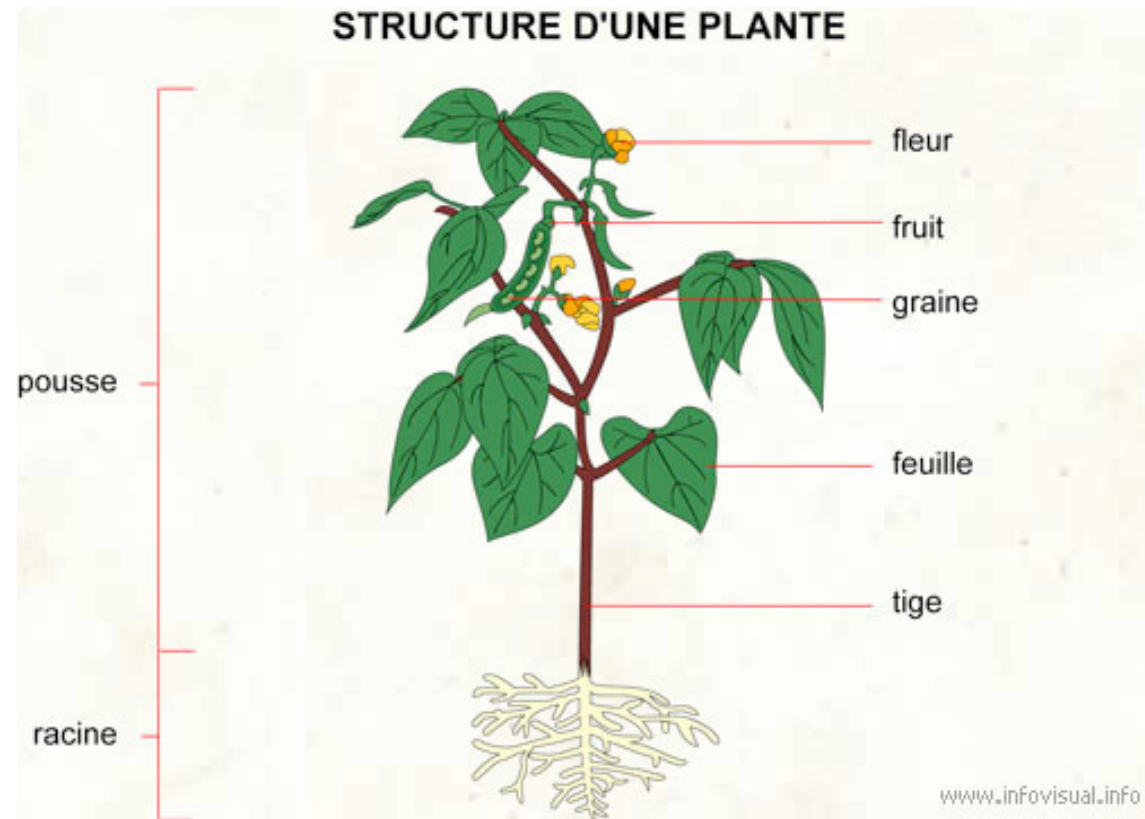
The models of biosystems are often not identifiable

Example : Monod model



$S(0)$	μ_{max}	K_S
7	1.1	1.8
11.6	1.0	6.8
18.2	0.7	12.9
25	0.3 (± 0.2)	7 (± 12)

Example : plant growth



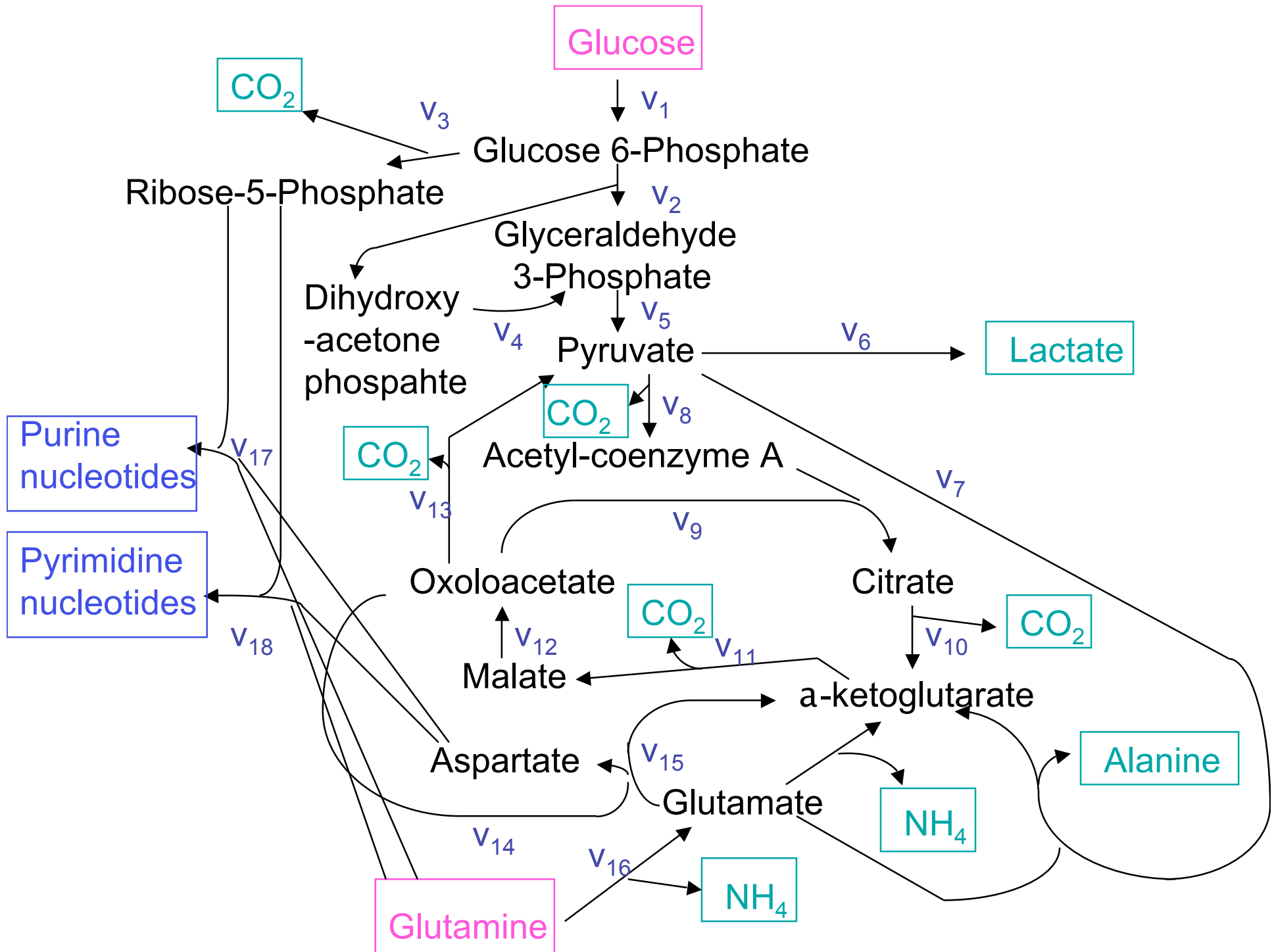
Main reactions : photosynthesis, (photo)respiration

How to better account for the cell complexity and its interactions with the medium?

- Metabolic engineering (and “system biology”)
- Population balance
- Microbial ecology

Link between reaction networks and metabolic engineering

- **Metabolic engineering** : complex reaction networks including the cell metabolism
- **Challenge** : can we validate metabolic pathways on the basis of a limited number of measured components while preserving the orientation (sign) of the reactions?
- **Solution** : convex basis
- **One (simple) example** : animal cells (CHO)
- **One challenge** : link between the wine quality and the reaction network of the production of organoleptic components (European project CAFE)



Reaction scheme of the CHO cells

- Metabolism : utilization of 2 main energetic nutrients
(metabolism of the amino-acids provided by the culture medium : neglected)
- 2 initial substrates : glucose and glutamine
- 4 final extracellular products : lactate, alanine, NH_4 , CO_2
- 2 final intracellular metabolites :
purine and pyrimidine nucleotides
- 12 internal metabolites
- 4 fundamental pathways : glycolysis, glutaminolysis, TCA cycle,
synthesis of the nucleotides

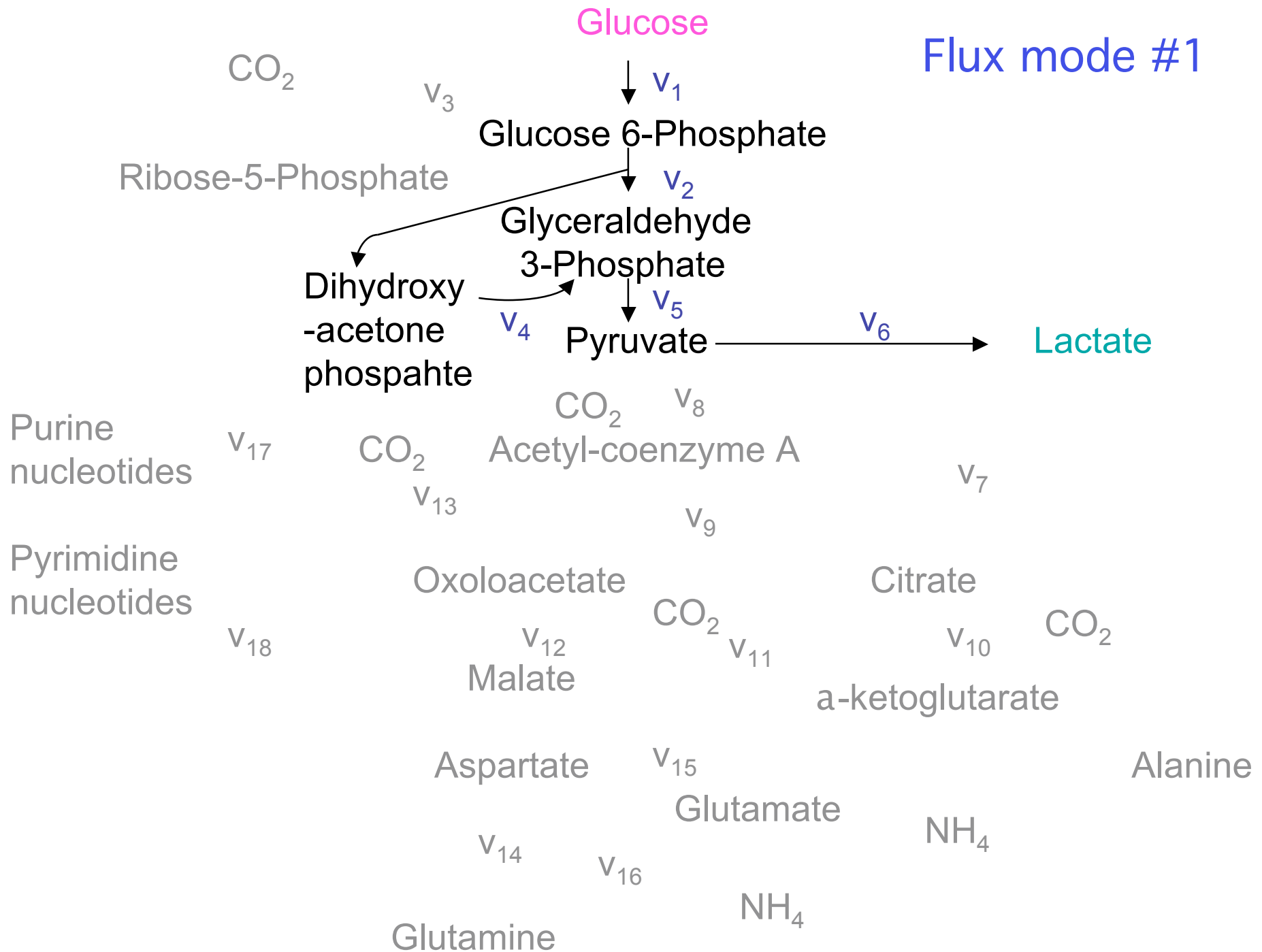
Metabolic flux analysis

- QSS approximation : $Kr = 0$ ($\dim(r) = 18$)
- reaction rates of the extracellular species (measured) : $Pr = r_m$
- Convex bases (\rightarrow values of positive fluxes) :
here : 7

\rightarrow 7 macroscopic reactions :

- 1) Glucose \rightarrow 2 Lactate
- 2) Glucose \rightarrow 6 CO_2
- 3) Glutamine \rightarrow Alanine + 2 CO_2 + NH_4
- 4) Glutamine \rightarrow Lactate + 2 CO_2 + NH_4
- 5) Glutamine \rightarrow 5 CO_2 + 2 NH_4
- 6) Glucose + 3 Glutamine \rightarrow Purine + 2 CO_2 + NH_4
- 7) Glucose + 2 Glutamine \rightarrow Pyrimidine + 2 CO_2 + NH_4

Flux mode #1



Flux mode #1

- 1st vector of the convex basis : $e_1 = [1 \ 1 \ 0 \ 1 \ 2 \ 2 \ 0 \ \dots \ 0]^T$

- In other words :

v_1 : Glucose \rightarrow Glucose6P

v_2 : Glucose6P \rightarrow DihydroxyacetoneP + Glyceraldehyde3P

v_4 : DihydroxyacetoneP \rightarrow Glyceraldehyde3P

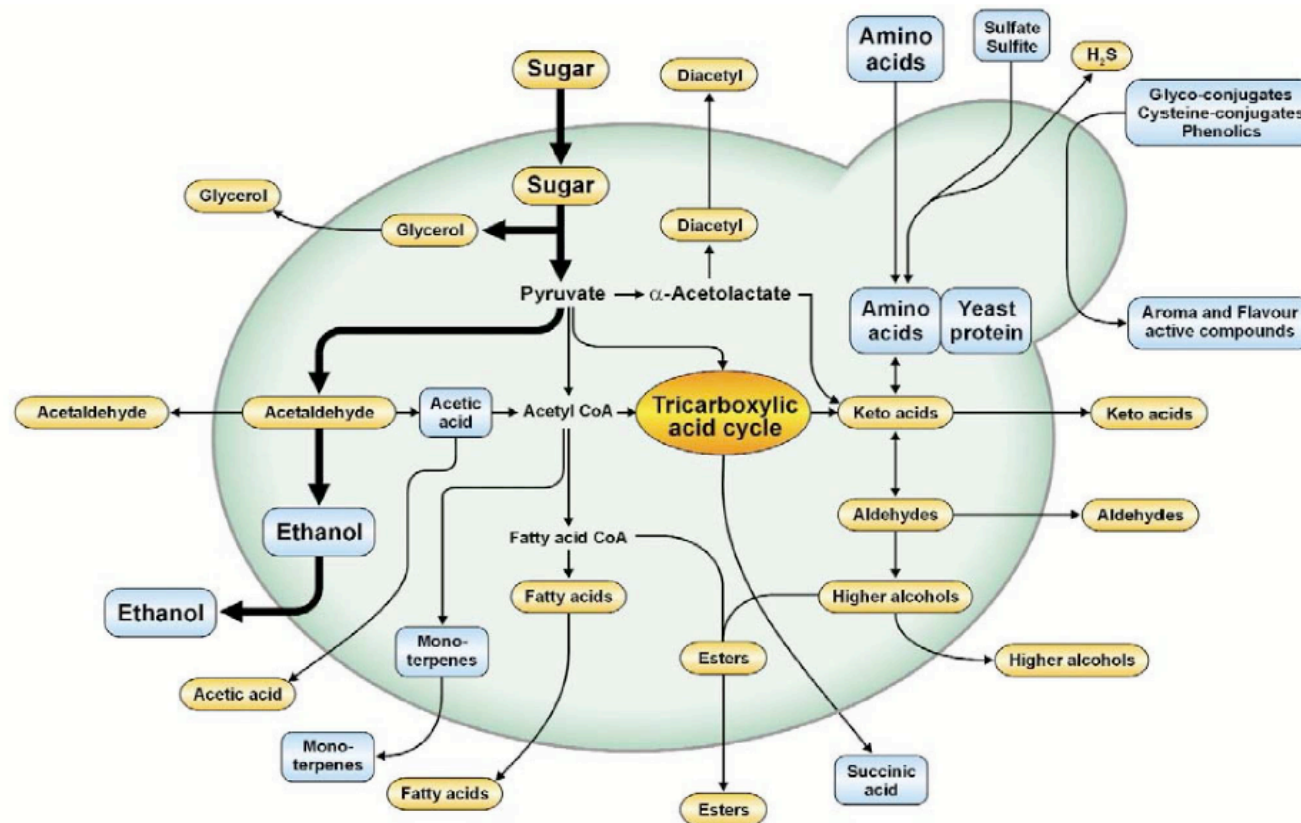
v_5 : Glyceraldehyde3P \rightarrow 2 Pyruvate

v_6 : 2 Pyruvate \rightarrow 2 Lactate

- Associated macroscopic reaction :

Glucose \rightarrow 2 Lactate

A more complex application : wine production

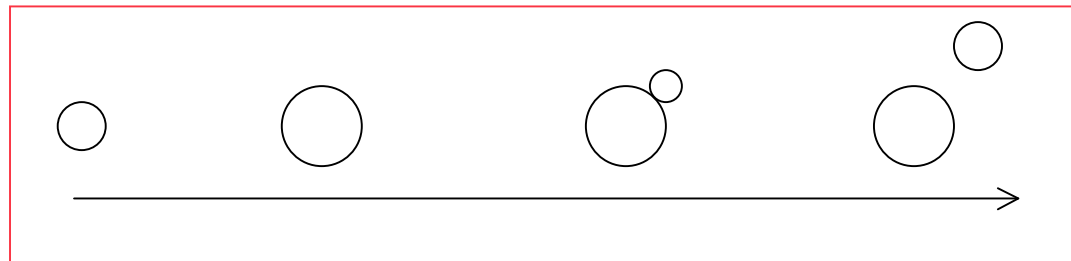


Challenge : how to transfer in simple models the synthesis of the indicators of the wine quality (amino-acids, sulfur compounds,...)

Population balance

--> Age distribution of the micro-organisms

Example : yeast



Budding (mother - daughter)

- $N(m, t)$: number of cells of mass m at time t per unit volume (cell density)

- **Total number** : $N_t(t) = \int_{m_{min}}^{m_{max}} N(m, t) dm$

- **Total concentration** : $X(t) = \int_{m_{min}}^{m_{max}} mN(m, t) dm$

- Balance equation :

$$\frac{\partial N}{\partial t} = \underbrace{-\frac{\partial r(m, S)N}{\partial m}}_{\text{growth rate}} - \underbrace{\Gamma(m, S)N}_{\text{rate of cellular division}} - DN + 2 \int_m^{m_{max}} \Gamma(m', S) p(m, m', S) N dm'$$

Microbial ecology

Issues and challenges

- Coexistence/competition are not just limited to ecology...
- The knowledge of the dynamical mechanisms of coexistence/competition of microbial species can be helpful for improving the running of industrial biological processes, e.g. :
 - Invasion of a culture by a contaminant
(Can we avoid systematic re-inoculation?)
 - Mixed cultures, e.g. :
 - * Lactic fermentation (*L. bulgaricus* vs *S. thermophilus*)
 - * Anaerobic digestion (*thermophilic* vs *mesophilic* bacteria)

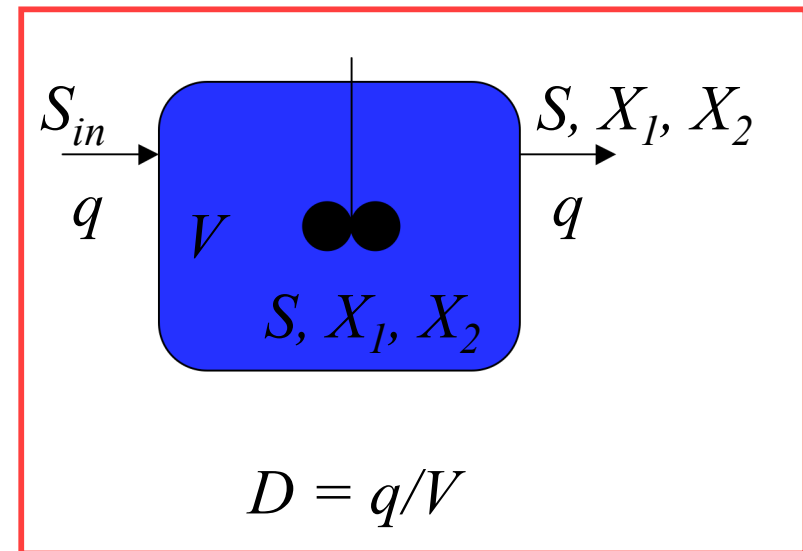
Competitive exclusion principle

Consider a continuous reactor
(« chemostat »)
with 2 species X_1 and X_2
sharing only one resource S :

$$\frac{dX_1}{dt} = \mu_1(S)X_1 - DX_1$$

$$\frac{dX_2}{dt} = \mu_2(S)X_2 - DX_2$$

$$\frac{dS}{dt} = -\frac{1}{Y_1}\mu_1(S)X_1 - \frac{1}{Y_2}\mu_2(S)X_2 + D(S_{in} - S)$$

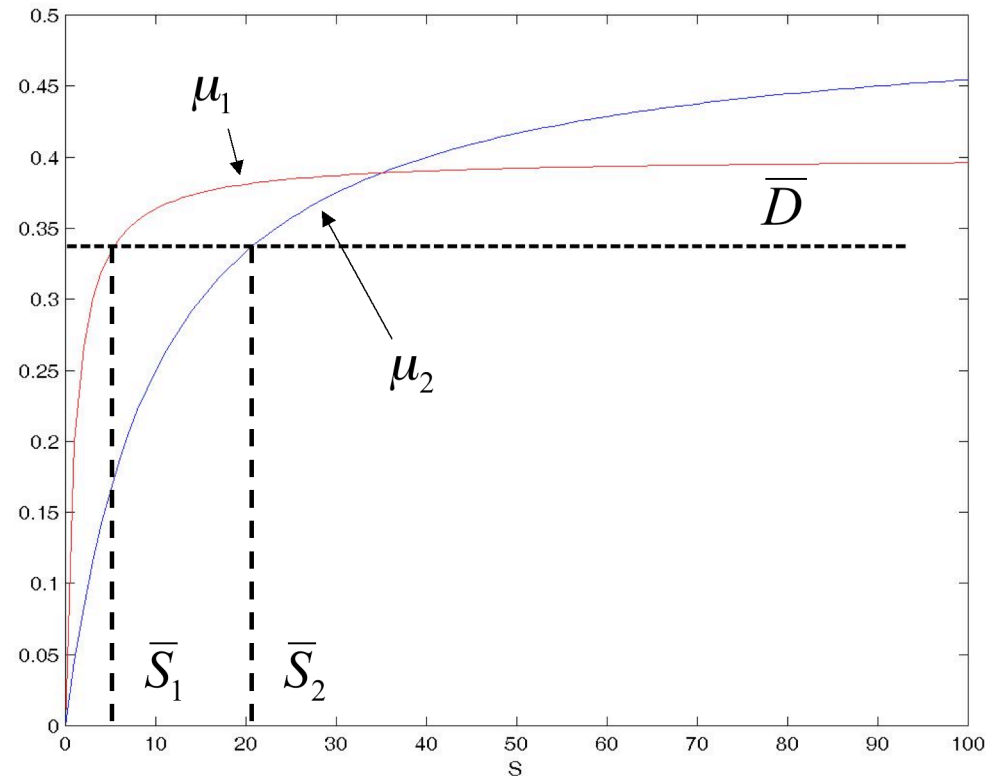


- At equilibrium : $\bar{\mu}_1(S) = \bar{\mu}_2(S) = \bar{D}$
 (only valid for specific values of D)
- In general, only one species «will win the competition and will survive» : --> growth curve that first intersects D
 («best affinity» or «lowest break-even concentration»)

- Here :

$$\bar{X}_1 = Y_1(S_{in} - \bar{S}), \bar{X}_2 = 0$$

(Hardin, 1960; Butler & Wolkowicz, 1985)



(Extension to n species and other growth curves)

Competitive exclusion principle : experimental validation

X_{A1} : *E. coli* (1)
 X_{A2} : *E. coli* (2)
 X_B : *P. aeruginosa*

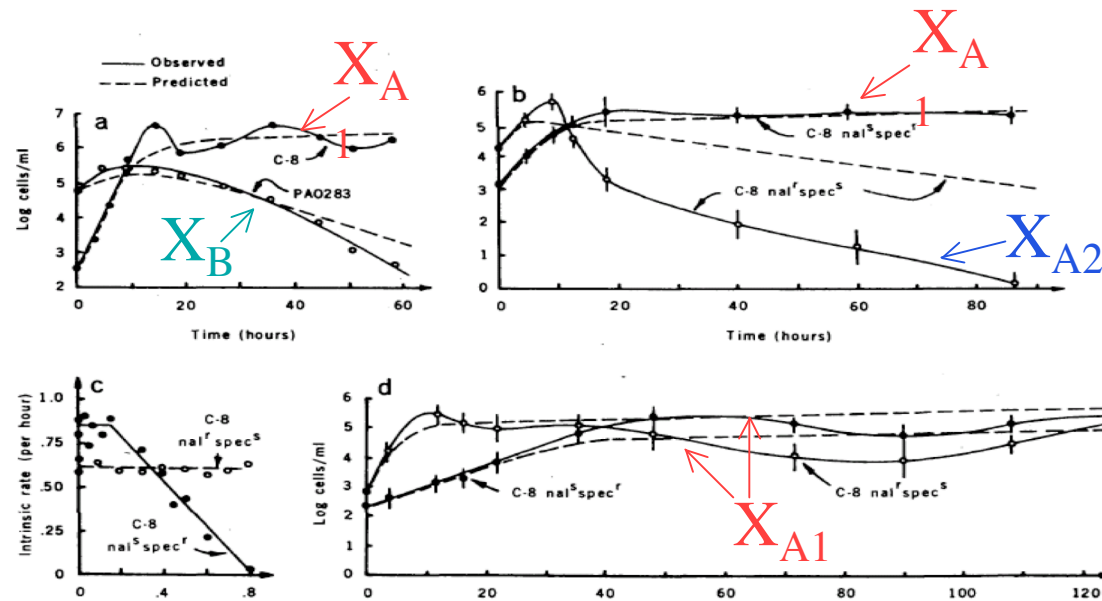
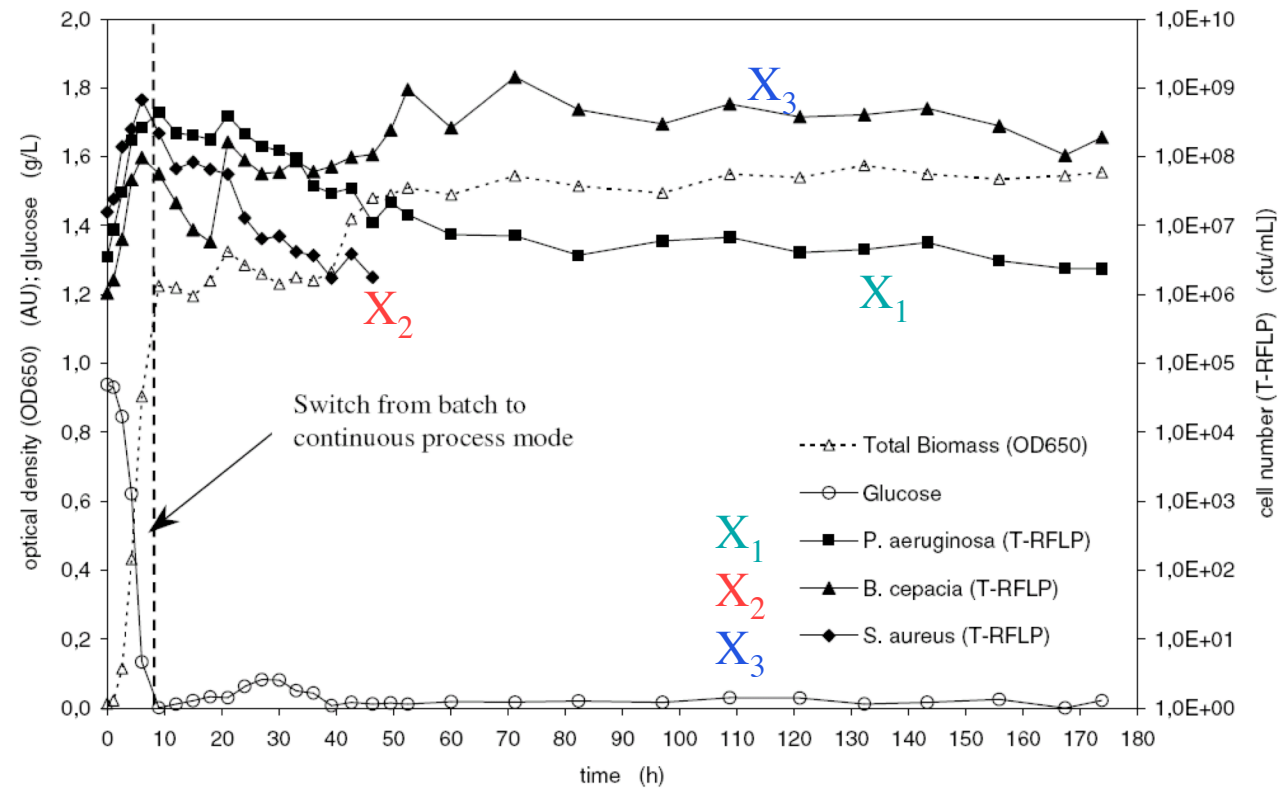


FIG. 5.2 – Validation qualitative expérimentale du comportement du modèle. Les prédictions qualitatives du modèle sont vérifiées pour : a) 2 espèces (*Escherichia coli*, souche C-8 et *Pseudomonas aeruginosa*, souche PA0283) qui diffèrent par leur constante de demi-saturation. b) 2 souches de *Escherichia coli* qui diffèrent par leur taux de croissance maximal. d) Coexistence obtenue avec 2 souches de *Escherichia coli* qui ont le même paramètre J_i . La figure c) représente l'effet de l'acide nalidixique sur le taux de croissance maximal pour les souches considérées C-8. D'après Hansen et Hubbell (1980).

The coexistence of different species is often observed

experimental evidence :



Schmidt, J. K., B. König et U.Reichl Characterization of a three bacteria mixed culture in a chemostat: Evaluation and application of a quant

Dynamical persistence

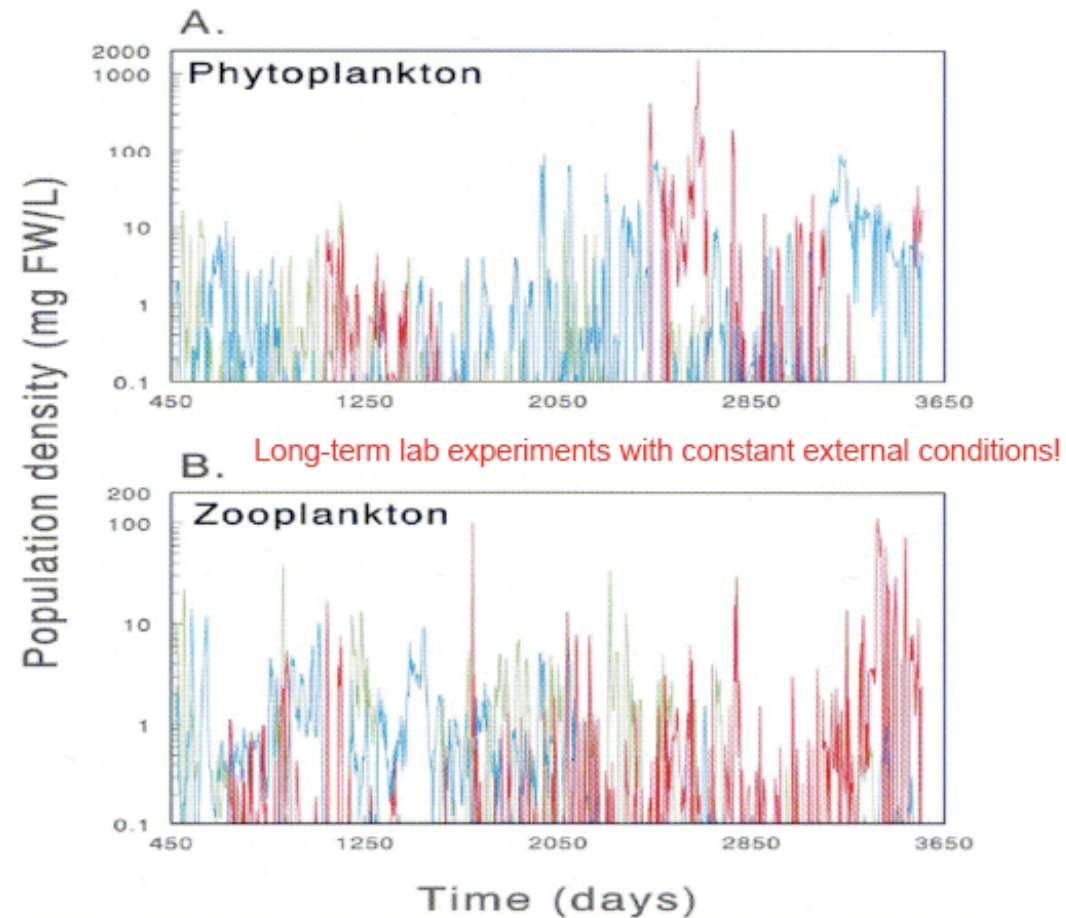


Figure 5. Non-equilibrium dynamics observed in an experimental multispecies community. The community developed in a long-term laboratory experiment under constant external conditions, and consisted of more than 20 different species. Data show the observed time course of (A) the dominant phytoplankton groups (green = green flagellates, blue = prokaryotic picc-phytoplankton, red = the diatom *Melosira*), and (B) the dominant zooplankton groups (green = the rotifer *Brachionus*, blue = the copepod *Eurytemora*, red = protozoans). Data were kindly provided by Hoerklöss (unpublished), and by Hoerklöss & Klinkenberg (1998), with permission from Schweizerbart'sche Verlagsbuchhandlung.

Model Properties

- Basic structural property
 - reaction invariant
- Model reduction
 - singular perturbations
- Stability
 - BIBS stability
 - unstable equilibrium points
- Observability & Controllability
- Non minimum phase (inverse response)

Basic Structural Property

Definition : $p = \text{rank}(K)$

→ K_a : a $(p \times M)$ full rank arbitrary matrix of K
 K_b : the remaining submatrix of K
 (x_a, x_b) , (Q_a, Q_b) and (F_a, F_b) the partitions of x , Q and F
induced by (K_a, K_b)

$$\rightarrow \begin{cases} \frac{dx_a}{dt} = K_a r(x_a, x_b) - Dx_a + F_a - Q_a \\ \frac{dx_b}{dt} = K_b r(x_a, x_b) - Dx_b + F_b - Q_b \end{cases}$$

Property

There exists a state transformation :

$$Z = A_0 x_a + x_b$$

where A_0 is the unique solution of the matrix equation :

$$A_0 K_a + K_b = 0 \quad \dim(A_0) = (N-p) \times p$$

such that the general dynamical model is equivalent to :

$$\begin{aligned} \frac{dx_a}{dt} &= K_a r(x_a, Z) - D x_a + F_a - Q_a \\ \frac{dZ}{dt} &= -D Z + F_b - Q_b + A_0 (F_a - Q_a) \end{aligned}$$

Remark : dynamics of Z independent of r

Example : PHB

- «Global» model with CO_2 (P_2) as a product in both reactions

$$x = \begin{bmatrix} X \\ S \\ N \\ P \\ C \\ P_2 \end{bmatrix}, \quad K = \begin{bmatrix} 1 & 0 \\ -k_1 & -k_5 \\ -k_2 & 0 \\ k_3 & 1 \\ -k_4 & -k_6 \\ k_7 & k_8 \end{bmatrix}, \quad r = \begin{bmatrix} \mu X \\ \nu X \end{bmatrix}$$

- One possible state partition

$$x_a = \begin{bmatrix} X \\ S \end{bmatrix} \quad x_b = \begin{bmatrix} N \\ P \\ C \\ P_2 \end{bmatrix}$$
$$\rightarrow K_a = \begin{bmatrix} 1 & 0 \\ -k_1 & -k_5 \end{bmatrix} \quad K_b = \begin{bmatrix} -k_2 & 0 \\ k_3 & 1 \\ -k_4 & -k_6 \\ k_7 & k_8 \end{bmatrix}$$

$$A_0 = \frac{1}{k_5} \begin{bmatrix} k_2 k_5 & 0 \\ -k_3 k_5 + k_1 & 1 \\ k_4 k_5 - k_1 k_6 & -k_6 \\ -k_5 k_7 + k_1 k_8 & k_8 \end{bmatrix}$$

$$Z = \begin{bmatrix} Z_1 \\ Z_2 \\ Z_3 \\ Z_4 \end{bmatrix} = \begin{bmatrix} k_2 X + N \\ - \left(k_3 + \frac{k_1}{k_5} \right) X + \frac{1}{k_1} S + P \\ - \left(k_4 + \frac{k_1 k_6}{k_5} \right) X + \frac{k_6}{k_1} S + C \\ - \left(k_7 - \frac{k_1 k_8}{k_5} \right) X + \frac{k_8}{k_1} S + P_2 \end{bmatrix}$$

Usually any partition is OK, but ...

Usually

- $\dim(K) = M$

(OK if the reactions are independent)

- the process components are “independent”

→ any choice of state partition is OK

- but not always : e.g. PHB (RQ = 1
--> C and P_2 are dependent))
IWA model (activated sludge model)

IWA model (reaction network)

1. Aerobic growth of heterotrophs : $S_S + S_O + S_{NH} \rightarrow X_{B,H}$
2. Anoxic growth of heterotrophs : $S_S + S_{NO} + S_{NH} \rightarrow X_{B,H}$
3. Aerobic growth of autotrophs : $S_O + S_{NH} \rightarrow X_{B,A} + S_{NO}$
4. Decay of heterotrophs : $X_{B,H} \rightarrow X_P + X_S + X_{ND}$
5. Decay of autotrophs : $X_{B,A} \rightarrow X_P + X_S + X_{ND}$
6. Ammonification of soluble organic nitrogen : $S_{ND} \rightarrow S_{NH}$
7. Hydrolysis of entrapped organics : $X_S \rightarrow S_S$
8. Hydrolysis of entrapped organic nitrogen : $X_{ND} \rightarrow S_{ND}$

There is a loop in the reaction network

- 8 reactions, 10 components
- Loop with reactions 1, 4 and 7

$$\longrightarrow \text{ if } x_a = [S_s, X_s, X_{B,H}, X_{B,A}, X_P, S_0, S_{NO}, S_{NH}]^T$$

then K_a is not full rank

- OK if S_{ND} or X_{ND} are included in x_a

homework : check it!

IWA model (reaction network)

1. Aerobic growth of heterotrophs : $S_S + S_O + S_{NH} \rightarrow X_{B,H}$
2. Anoxic growth of heterotrophs : $S_S + S_{NO} + S_{NH} \rightarrow X_{B,H}$
3. Aerobic growth of autotrophs : $S_O + S_{NH} \rightarrow X_{B,A} + S_{NO}$
4. Decay of heterotrophs : $X_{B,H} \rightarrow X_P + X_S + X_{ND}$
5. Decay of autotrophs : $X_{B,A} \rightarrow X_P + X_S + X_{ND}$
6. Ammonification of soluble organic nitrogen : $S_{ND} \rightarrow S_{NH}$
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8. Hydrolysis of entrapped organic nitrogen : $X_{ND} \rightarrow S_{ND}$

Model Reduction

- Singular perturbation : ODE \rightarrow algebraic equation

- Low solubility product P : $\frac{dP}{dt} = kr - DP - Q$



$$P = \Pi P_{sat}$$

$$\rightarrow \frac{dP}{dt} = kr - D\Pi P_{sat} - Q$$

$$P_{sat} \rightarrow 0 \Rightarrow Q = kr$$

Substrates in fast reactions (only)

Example : two sequential reactions : $A \rightarrow B, B \rightarrow C$

Kinetics : $r_1 = \gamma_1 A \alpha_1(A,B), r_2 = \gamma_2 B \alpha_2(B,C), \quad \gamma_1, \gamma_2 > 0$

Assumption : reaction 2 fast and reaction 1 slow, i.e. $\gamma_1 \ll \gamma_2$

Define : $\epsilon = \frac{1}{\gamma_2}$ and $Z = C + \frac{k_4}{k_3} B$

$$\rightarrow \epsilon \frac{dB}{dt} = -\epsilon DB + \epsilon k_2 \gamma_1 A \alpha_1 - k_3 \alpha_2 B \quad \epsilon \rightarrow 0 : B \rightarrow 0$$

$$\rightarrow \frac{dZ}{dt} = \left(\frac{dC}{dt} \right) = -DZ + \frac{k_1 k_4}{k_3} r_1 = -DC + \frac{k_1 k_4}{k_3} r_1$$

General rule for model reduction

- $\frac{dx}{dt} = 0$ and $x = 0$
- Quasi-steady state (QSS) approximation

Stability Analysis

1. BIBS stability

- BIBS : bounded input bounded state
- Motivation : - is the model in accordance with the physical reality?
- under which conditions?
- Assumptions :
 - A1. $0 < D_{min} \leq D(t)$
 - A2. $0 \leq F_i(t) \leq F_{max}$
 - A3. Principle of Mass Conservation :
 $\exists \gamma > 0$ such that $\gamma^T K_j = 0$, for all j (K_j : j^{th} column of K)
- Theorem : $0 \leq \mathbf{x}(t) \leq \mathbf{x}_{max}$

Rewriting of the Model Equations

- **Reaction rates** : $r_j(x) = \alpha_j(x) \left(\prod_{j \cap n} x_n \right)$, $0 \leq \alpha_j(x) \leq \alpha_{max}$
reactants and autocatalyst
in reaction j

Example : growth rate μX with a Monod model

$$\alpha_j(x) = \frac{\mu_{max}}{K_S + S}, \quad \left(\prod_{j \cap n} x_n \right) = SX$$

- **Gaseous outflow rates** : $Q_i = \beta_i x_i$, $0 \leq \beta_i$, $0 \leq x_i \leq x_{is}$
- **Feed rates (liquid phase)** : $F_i = DS_{i,in}$

Proof :

a) $x_i(t) \geq 0$

$$\frac{dx_i}{dt} = \sum_j (+)k_{ij}r_j + F_i \geq 0$$

b) $x_i(t) \leq x_{max}$

Define $z = \gamma^T x$

$$\text{Then : } \frac{dz}{dt} = -Dz - \gamma^T Q + \gamma^T F \leq -Dz + \gamma^T F_{max}$$

$$\Rightarrow z \leq \frac{\gamma^T F_{max}}{D_{min}} \Rightarrow x_i \leq \frac{\gamma^T F_{max}}{\gamma_i D_{min}} \quad \forall i$$

- Remarks :
- if $F_i = DS_{i,in}$ (liquid substrates) : $z \leq \gamma^T S_{in}$
 - alternative (more complex) proofs

Example : PHB

$$K = \begin{bmatrix} 1 & 0 \\ -k_1 & -k_5 \\ -k_2 & 0 \\ k_3 & 1 \\ -k_4 & -k_6 \\ k_7 & k_8 \end{bmatrix}$$

--> one possible choice for γ : $\gamma =$

$$\begin{bmatrix} \frac{k_1 k_8}{2k_5 k_7} + \frac{k_4}{2k_3 k_6} \\ \frac{k_8}{2k_5 k_7} \\ \frac{1}{k_2} \\ \frac{1}{2k_3} \\ \frac{1}{2k_2 k_6} \\ \frac{1}{k_7} \end{bmatrix}$$

2. Asymptotic Stability

Equilibrium points

- Definition : constant state such that : $\frac{d\bar{x}}{dt} = 0$
 - these are solutions of the algebraic equation :

$$-\bar{D}\bar{x} + Kr(\bar{x}) + \bar{F} - \bar{Q} = 0$$

- Specificity of (bio)chemical process models : multiple steady-state :

One value of $(\bar{D}, \bar{F}) \Rightarrow$ multiple values for \bar{x}

A simple example

- $S \longrightarrow X$
- Dynamical equations in steady state :

$$\frac{d\bar{S}}{dt} = 0 \quad \rightarrow \quad -k_1\bar{\mu}\bar{X} + \bar{D}\bar{S}_{in} - \bar{D}\bar{S} = 0 \quad (1)$$

$$\frac{d\bar{X}}{dt} = 0 \quad \rightarrow \quad (\bar{\mu} - \bar{D})\bar{X} = 0 \quad (2)$$

- From (2), 2 possible solutions (equilibrium points) :

1) $\bar{\mu} = \bar{D}$

2) $\bar{X} = 0$ (and $\bar{S} = \bar{S}_{in}$) (Wash-out)
(the only possible if $\bar{D} > \mu_{max}$)

- The explicit solution of 1) requires a model for μ

- **Monod model** : $\mu = \frac{\mu_{max}S}{K_S + S}$

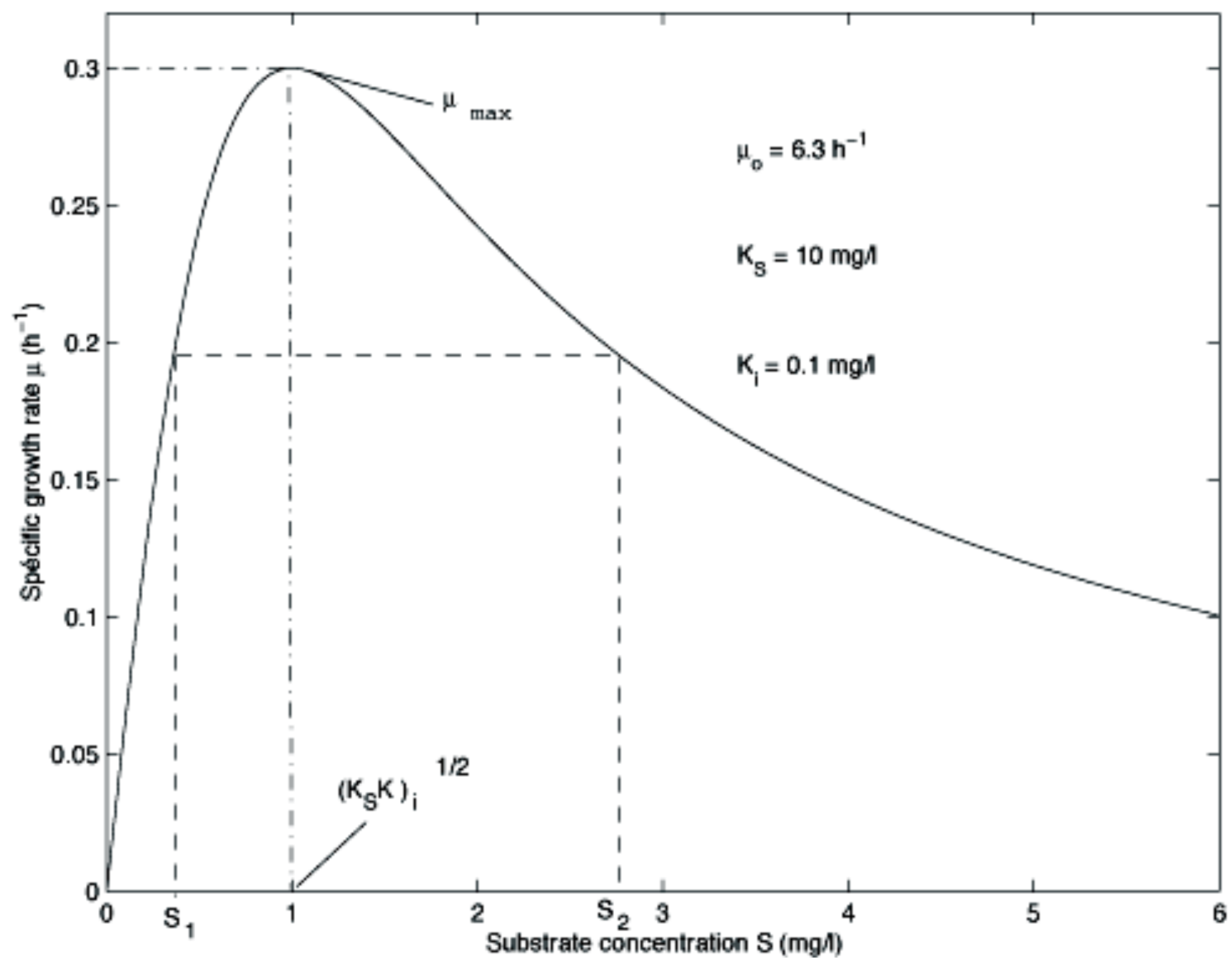
Equilibrium point 1) : $\bar{S} = \frac{\bar{D}}{\mu_{max} - \bar{D}}, \bar{X} = \bar{S}_{in} - \bar{S}$

- **Haldane model (inhibition)** : $\mu = \frac{\mu^*S}{K_S + S + \frac{S^2}{K_I}}$

2 possible solutions to 1) (i.e. 3 equilibrium points) :

$$1) \bar{S}_1 = \frac{\mu^* - \bar{D}}{2\bar{D}}K_I - \frac{K_I}{2} \sqrt{\left(\frac{\mu^*}{\bar{D}} - 1\right)^2 - 4\frac{K_S}{K_I}}$$

$$2) \bar{S}_2 = \frac{\mu^* - \bar{D}}{2\bar{D}}K_I + \frac{K_I}{2} \sqrt{\left(\frac{\mu^*}{\bar{D}} - 1\right)^2 - 4\frac{K_S}{K_I}}$$



Stability of the equilibrium points

- Linearized tangent model (around equilibrium points) :

$$\frac{d}{dt}(x - \bar{x}) = A(\bar{x}, \bar{D}, \bar{F})(x - \bar{x}) - \bar{x}(D - \bar{D}) + (F - \bar{F})$$

with $A(\bar{x}, \bar{D}, \bar{F}) = K \left[\frac{\partial r}{\partial x} \right]_{x=\bar{x}} - \bar{D}I_N$

- Lyapunov's stability first method : eigenvalues of A ($\lambda_i(A)$) :

If $Re(\lambda_i(A)) < 0$ for all i , then the equilibrium point is stable

Example : Haldane model

$$A(\bar{x}, \bar{D}, \bar{F}) = \begin{bmatrix} 0 & \Omega \\ -k_1 \bar{D} & -k_1 \Omega - \bar{D} \end{bmatrix}$$

with $\Omega = \frac{\mu^* \bar{X} \left(K_S - \frac{\bar{S}^2}{K_I} \right)}{\left(K_S + \bar{S} + \frac{\bar{S}^2}{K_I} \right)^2}$

Eigenvalues of A : $Det(\lambda I - A) = \lambda^2 + \lambda(k_1 \Omega + D) + k_1 \Omega D = 0$

$$\text{---> } \lambda_1 = -D, \lambda_2 = -k_1 \Omega$$

$$\text{---> stable if } \bar{S} < \sqrt{K_S K_I}$$

$$\text{unstable if } \bar{S} > \sqrt{K_S K_I}$$

Observability and Controllability

- Based on the linearized tangent model (sufficient conditions)

$$\frac{d}{dt}(x - \bar{x}) = \left(K \left[\frac{\partial r}{\partial x} \right]_{x=\bar{x}} - \bar{D}I_N \right) (x - \bar{x}) - \bar{x} (D - \bar{D}) + (F - \bar{F})$$

- **Observability** : p measured components

\mathbf{O} = observability matrix

$$\rightarrow \text{rank}(\mathbf{O}) \leq \min\{N, p+M\}$$

- **Controllability** : q control inputs

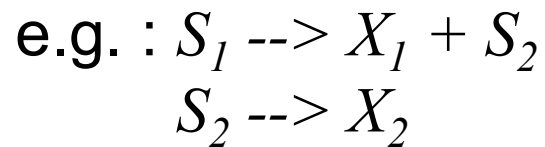
\mathbf{C} = controllability matrix

$$\rightarrow \text{rank}(\mathbf{C}) \leq \min\{N, q+M\} \quad (\text{if only feedrates } F)$$

$\rightarrow \text{rank}(\mathbf{C})$ increased by one with D as an additional input
except at equilibrium points

Non Minimum Phase (Inverse Response)

- NMP = « unstable » zeros
- Time response : first in a direction inverse to the final response
- Already for reaction networks with two sequential reactions.



---> transfer function of the linearized tangent model
between D and S_2 :

$$H(s) = \frac{s - \frac{k_1 k_2 \bar{\mu}_{1S} \bar{X}_1 \bar{X}_2}{\bar{S}_2}}{(s + k_1 \bar{\mu}_{2S} \bar{X}_1) (s + k_1 \bar{\mu}_{2S} \bar{X}_2)}$$

Laplace Transform

Example : reactant in a first-order reaction

$$\frac{\partial C}{\partial t} = -u \frac{\partial C}{\partial z} - k_0 C, \quad C(z = 0, t) = C_{in}(t)$$

Laplace transform with respect to t :

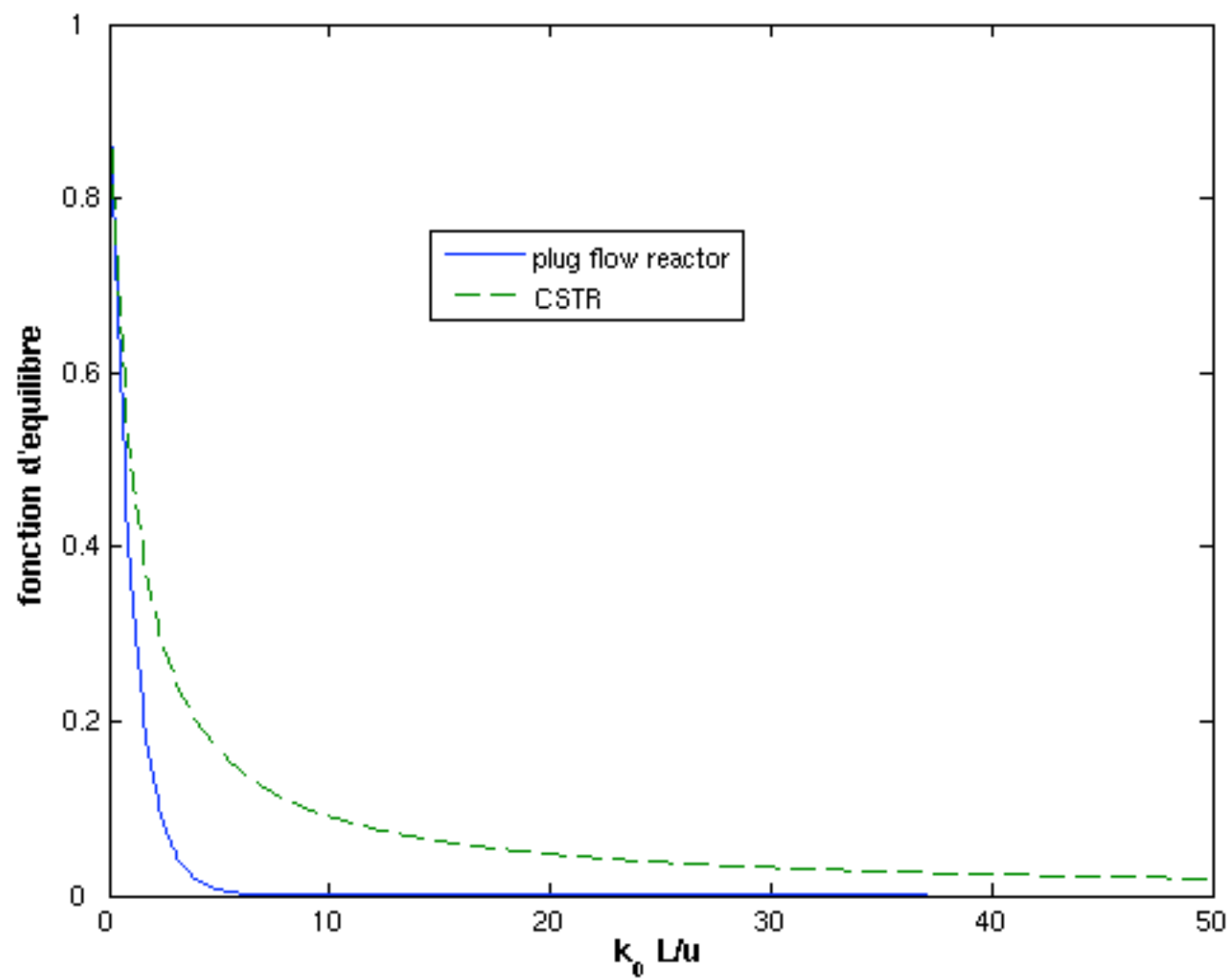
$$sC(z, s) = -u \frac{\partial C}{\partial z} - k_0 C \quad \rightarrow \quad \frac{\partial C}{\partial z} = -\frac{s + k_0}{u} C$$

- Solution : $C(z, s) = \underbrace{C(0, s)}_{\text{steady-state}} e^{-\frac{k_0 z}{u}} e^{-\frac{sz}{u}}_{\text{delay !}}$

$$C(0, s) = C_{in}$$

- CSTR : steady-state : $\bar{C} = \frac{C_{in}}{1 + \frac{k_0}{D}} \quad \left(D = \frac{u}{L} \right)$

→ Plug flow reactor \approx CSTR + time delay



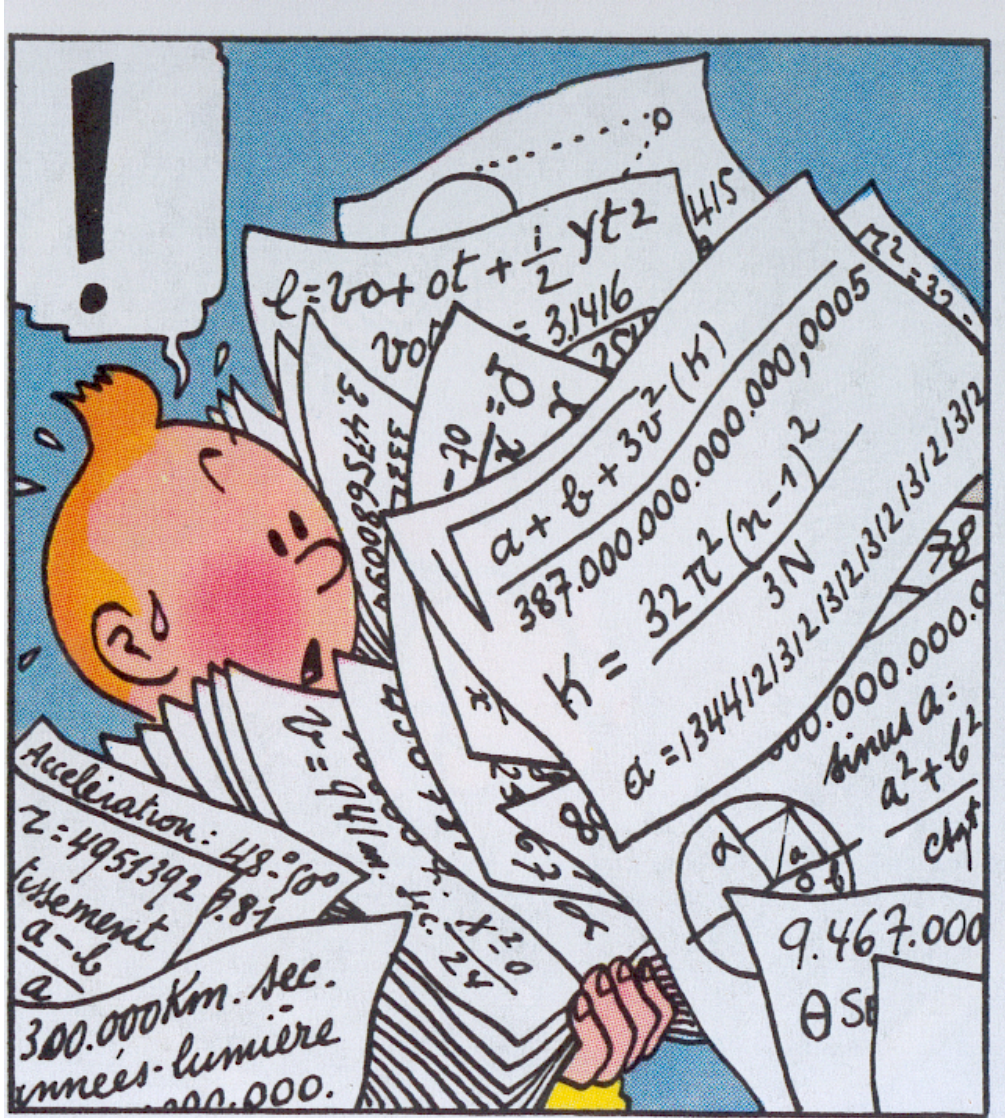
Challenges

- Complex reaction network
- Living organisms : their behaviour changes with time
- Kinetics badly known (mixture of complex biochemical kinetics and (auto-)catalytic reactions (multi-phase))

-> Complex high order nonlinear models

- Few available (on-line and off-line) measurements

-> Difficult to obtain reliable models



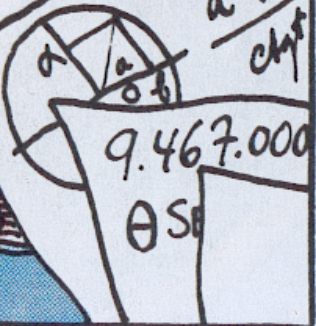
Accelération: 48.500
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 a
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 $000.000.$

$$l = v_0 t + at + \frac{1}{2} yt^2$$

$v_0 = 3,1416$
 415

$$a + b + 3v^2 (K)$$

$387.000.000.000.000,0005$
 $h = \frac{32\pi^2 (n-1)^2}{3N}$
 $a = 1344121312131213121312$



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